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# MEMBRANE BIOREACTOR APPLIED TO THE TREATMENT OF A FRUIT PROCESSING INDUSTRY WASTEWATER IN NORTHEAST BRAZIL

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#### Abstract

The market for Membrane Bioreactors (MBR) technology has recently grown due to increasingly strict standards for effluent discharge and the need for alternative water sources. The high quality of the effluent produced, enabling the possibility of reuse is one of the most attractive characteristics of this technology. The objective of this article was to evaluate the treatment efficiency of a pilot-scale MBR plant in a fruit processing industry, including an analysis of the possibilities for effluent reuse. The pilot plant comprised a MBR with approximately 5000L in capacity, with porous type ultrafiltration grade polyethersulfone membranes. Other details for the membranes were: submerged configuration, flat plate type geometry, pore diameter ranging from 0.035 to 0.1 µm and total area of 25m<sup>2</sup>. The industrial effluent came from fruits processing, floors and machinery washing, and was characterized by physical, chemical and bacteriological parameters. Results showed that permeability decreased about 50% during the monitoring, indicating the need of membrane cleaning. The removal efficiency for COD, BOD<sub>5</sub>, total nitrogen and total phosphorus, was 97.1%, 98.7%; 95.7 % and 53.5%, respectively. There was an absence of both total coliform and <u>E</u>. <u>Coli</u> at the inlet and outlet of the system. The permeate fits into agricultural, urban, environmental, industrial and aquaculture reuse modalities.

Keywords: industrial effluents, mbr, reuse, water scarcity, ultrafiltration.

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#### Introduction

A depletion of water resources coupled with population growth results in a water crisis in both quantitative and qualitative terms (Sehar and Nasser, 2019). Moreover, increasing industrial demand increases the generation of industrial wastes. Food industry wastewaters are a significant source of pollution of water resources due to the large amounts and variety of pollutants they contain (Sawadogo *et al.*, 2018).

As in other food industries, fruit processing companies use water in a range of steps (Mundi *et al.*, 2017; Moore *et al.*, 2016). Treatment of wastewater from fruit processing involves additional difficulties due to the high organic load, the chemicals used in the process and seasonal variations in pH and flow rates (Tekerlekopoulou *et al.*, 2020; Moore *et al.*, 2016). Moreover, strict standards for industrial effluent discharge into the environment, are becoming a greater challenge (Sehar and Nasser, 2019; Casani *et al.*, 2005). Regarding industrial wastewater treatment, conventional activated sludge (CAS) and membrane bioreactors (MBR) are the most commonly used technologies (Pirsaheb *et al.*, 2019). MBR technology has recently been gaining more attention than CAS due to more stringent discharge requirements and the need for effluent reuse (Khouni *et al.*, 2020; Andrade *et al.*, 2013).

The use of MBR for the treatment of wastewater has grown worldwide since the mid-1990s, both in quantity and in treatment capacity, since such technology has been at the forefront of technological advances, and has increasingly assumed a prominent position in the competitiveness of deployment and operation costs (Xiao *et al.*, 2019; Ziegler *et al.*, 2016; Grull, 2013; Santos *et al.*, 2011).

Moreover, the existence of competitive MBR suppliers (Qiblawey and Judd, 2019), as well as the accumulation of operational data through academic and field studies (Park *et al.*, 2015) has accelerated the application of MBR technology, so that large plants are currently in operation. Xiao *et al.*, (2019) reports on an MBR plant under expansion phase in Sweden, that when finished, will be the largest plant of this kind in the world, with treatment capacity of 864.000 m<sup>3</sup>.d<sup>-1</sup>.

The development of submerged membranes has taken MBR applicability to a new level, considering that they require much less energy to function, can be adapted to larger systems and make costs competitive with conventional wastewater treatment technologies (Grull, 2013; Judd, 2006). In addition, the costs of replacing membrane modules have diminished and the replacement cycles of the modules are increasingly longer (Qiblawey and Judd, 2019; Baker, 2012). In this perspective, Qiblawey and Judd (2019) report that for even greater cost reduction, efficient pretreatment as well as system automation should be considered. Park et al. (2015) report that recent developments and improvements in membrane fouling control have led to more favorable projections of membrane life and significantly reduced overall operational and maintenance costs.



The main objective of MBR is to produce clarified and disinfected effluent (Judd, 2016). Investigations in MBR show that such processes present efficient and stable treatment of organic matter, nutrients, pathogens, besides presenting promising potential for the removal of emerging pollutants (Martí-Calatayud *et al.* 2020; Xiao *et al.*, 2019). Hao (2014) and Deowan *et al.* (2016) report that MBR technology has been increasingly used in the treatment of industrial wastewater since they produce a final effluent with quality compatible with several reuse options.

In Brazil, MBR technology is still considered emerging, with some research papers in the area and few applications on a real scale (Belli, 2015). Moreover, most studies with MBR focus on domestic wastewater treatment (Da Costa *et al.*, 2018; Belli *et al.*, 2017; Subtil *et al.*, 2013; Belli *et al.*, 2012). Regarding industrial wastewater, Andrade et al. (2013) evaluated MBR applied to the wastewater treatment of dairy industries. When it comes to MBR applied to the wastewater treatment of fruit processing industries, studies are still scarce.

In this context, this study aimed to evaluate the performance of a pitot-scale MBR in the treatment of the effluent in a fruit processing industry located in Northeast Brazil, as well as to verify the possibilities of reusing the treated effluent.

# **Materials and method**

# Description of the system

This study examined a MBR pilot-plant from the *Brazil Managed Aquifer Recharge Project* (BRAMAR). BRAMAR is a Brazil-Germany bilateral cooperation research project, and provided a pilot-scale treatment plant for use by a fruit processing company in João Pessoa-PB/Brazil, where the study was conducted. The wastewater produced by the company came from the washing and processing of fruits, as well as floor and machinery cleaning. The effluent drained by gravity through a channel to the place where the treatment plant was installed. A flowchart of the pilot plant is detailed in Figure 1.

Wastewater was collected with an eccentric pump, which drew the effluent from the channel through a 1 mm mesh sieve filter. The wastewater was then sent to a 1000L tank (equalization tank), with a mixer inside to avoid sedimentation and homogenize the effluent. Another eccentric pump, identical to the previous one, then passed the effluent from the equalization tank to the electroflotation tank. After electroflotation, a 200L tank (MBR feed tank) used an automatic level control that activated a drainage pump to feed the MBR tank.

The MBR tank had approximately 5000L capacity, with an immersed ultrafiltration membrane module. The membrane was porous, with pore diameter ranging from 0.035 to 0.1  $\mu$ m, and the membrane material was polyethersulphone (PES). The membrane geometry was flat plate type,



with submerged configuration and the total module area was 25m<sup>2</sup>. Three aerators were used, two to provide oxygen to the MBR tank and one for membrane scouring. Whenever the dissolved oxygen (DO) concentration reached values below 2 mg.L<sup>-1</sup>, the minimum recommended for biological treatment, aeration was triggered.



Figure 1. Scheme of the MBR pilot plant.

Finally, the treated effluent (permeate) was pumped by an eccentric pump to a tank with a capacity of 400L, which was used to collect the final effluent. The pilot plant had an ultrasonic flow meter (Flowmax 44i MIB GmbH). The MBR monitoring period was 4 months, between December 2016 and April 2017, a period preceded by a 15-day period of acclimatization. Average flow during the days of operation was 1.6 m<sup>3</sup>.day<sup>-1</sup>. During this period no chemical cleaning of the membrane was performed. In the acclimatization phase, sludge from an activated sludge plant was inoculated into the MBR module.

# Industrial wastewater characterization

For most of the time of operation the fruits processed in the industry were pineapple, acerola, mango and guava. MBR performance was evaluated by collecting samples from three distinct points: in the equalization tank (point 1), in the MBR feed tank (point 2) and in the permeate tank (point 3). A data acquisition system coupled to the *ACRON Reporter* software collected and stored the following parameters: pH, DO, temperature, mixed liquor level in the reactor and permeate



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flow and transmembrane pressure. The physical and chemical analyses performed were: Chemical Oxygen Demand (COD), Biological Oxygen Demand (BOD<sub>5</sub>), Total Suspended Solids (TSS), Total Nitrogen (TN), Total Phosphorus (TP), as well as measurements of pH, Temperature (T), and electric conductivity (EC) with the aid of a multiparameter probe (Hanna). Total coliform and *E. coli* tests were performed for the microbiological analysis.

Due to the high organic load it was necessary to add nitrogen and phosphorus in the reactor, since such nutrients were present in low concentration in the industrial effluent and are essential for the growth of bacteria. The lack of nitrogen and phosphorus is common in the treatment of effluents from food processing industries with high organic content (Metcalf & Eddy, 2016). Thus, rather than evaluating the efficiency of TN and TP removal, these parameters were of paramount need to calculate the necessary dosage of these nutrients to be added into the reactor, always seeking to maintain the COD:N:P ratio close to 200:5:1. Urea was used as a source of nitrogen and phosphoric acid and/or diamonium hydrogen phosphate as a source of phosphorus.

Parameter	Method				
COD	Closed reflux colorimetric method				
BOD <sub>5</sub>	Oxidirect (BOD System)				
TSS	APHA (2012)				
TN	HACH 10.071				
ТР	HACH 8.190				
EC	Hanna Combo waterproof pH/EC/TDS/Temp				
рН	Hanna Combo waterproof pH/EC/TDS/Temp				
Т	Hanna Combo waterproof pH/EC/TDS/Temp				
Total coliform and E.coli	APHA (2012) and Colilert				

 Table 1. Physical, chemical and microbiological analysis.

# **Results and discussion**

#### MBR operation and control

The volume of the reactor was controlled by a level sensor to operate between 87% and 94% of the total capacity. When the level reached 94%, the feeding was stopped, and when the level was at 88%, the feeding pump was turned on again. Along the monitoring period, the mean level in the reactor was 88.4% of the full capacity (Figure 2 – A). Levels lower than 87% occurred only at sludge discharge occasions.

With regard to TSS, the ideal band for the operation of MBR is considered as 8-12 g.L<sup>-1</sup> (Metcalf & Eddy, 2016; Park *et al.,* 2015), while the maximum value to avoid flux reduction due to fouling is



18 g.L<sup>-1</sup> (Metcalf & Eddy, 2016). In this study the MBR was operated with TSS between 12 and 18 g.L<sup>-1</sup>, as shown in Figure 2 (B). Sludge discharge actions were used to keep the TSS concentration under this mentioned range.



Figure 2. Level variation in the reactor (A) and TSS in the mixed liquor (B) along the monitoring period of the MBR.

The level in the reactor and the transmembrane pressure were used for permeability calculation. When reactor level was lower than 94%, an additional volume of 2.17% was used for the correction of the transmembrane pressure due to the liquor volume that was not occupying the reactor.

Figure 3 (A) shows that membranes' permeability decreased about 50% from the beginning to the end of the monitoring period, indicating the need for cleaning. Viero (2006) reports that the reduction on the effective filtration area, and consequently membrane permeability, is related to flux reduction, due to membrane fouling. Figure 3 (B) shows the initial flux of the membranes, between 13 and 15 L.m<sup>-2</sup>.h<sup>-1</sup>, where intermittent cycles of suction and relaxation were alternated (suction: 10 min.; relaxation: 2 min).

Temperature in the mixed liquor are presented in Figure 4 (A), where the values varied inside the ideal range of 25-35 °C (Jordão e Pessoa, 2011) for aerobic treatment processes. The mean temperature in the mixed liquor suspended solids (MLSS) was 29.7°C. Temperture is an important parameter in MBR performance, since it governs microbial metabolism (Park *et al.*, 2015).

Mean value for DO in the MLSS was 3.4 mg.L<sup>-1</sup>, which is above the minimum recommended value (Metcalf & Eddy, 2016; Moore *et al.*, 2016) of 2.0 mg.L<sup>-1</sup>. Low values of DO initially recorded are



due to the reduced active biomass in the MLSS, since the reactor was inoculated with sludge 15 days before the monitoring began. Figure 4 (B) shows DO concentration in the MLSS. Aeration was always turned on when DO was as low as 2.0 mg.L<sup>-1</sup>.



Figure 3. Membrane permeability (A) and operational strategy (B) along MBR monitoring period.



Figure 4. Temperature (A) and dissolved oxygen (B) in the MLSS along the MBR monitoring period.

Mean values of pH, temperature (T) and electric conductivity (EC) recorded for the three monitoring points (MP) are shown in Table 2. Initially, the values were recorded at different times along the day, and because there were no accentuated variations, the mean values were calculated for each day.



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able 2. Characterization of the industrial wastewater (MP1), eletroflotation effluent (MP2) and permeate (MP3).											
	MF	MP1 (wastewater, inlet)			MP2 (eletroflotation effluent)			MP3 (permeate)			
	рН	T (°C)	EC (mS/cm)	рН	T (°C)	EC (mS/cm)	рΗ	T (°C)	EC (mS/cm)		
Mean	4.5	32.0	1.9	4.9	32.5	2.1	7.9	33.1	2.2		

There was an increase on mean pH values from the industrial wastewater (4.5) to the permeate (7.9). Low pH values in the industrial wastewater are due to the type of fruits processed and to the acids used in the machinery cleaning operations. Moore (2015) also reported similar results, when pH rose from 4.9 in the influent wastewater to 8.0 in the MBR permeate, where it was

According to Brazilian legislation (CONAMA Resolution 430/2011), effluents of any source can be discharged in water bodies only if, among other conditions, pH is between 5 and 9 (Brasil, 2011). The mean pH values in the permeated complies with this discharge requirement and also with the recommendation of effluent quality for reuse according to NBR 13.969/1997 (ABNT, 1997) and COEMA Resolution 2/2017 (Ceará, 2017).

It can be noticed that EC did not varied significantly along the treatment phases (MP1, MP2 and MP3). According to Metcalf & Eddy (2016), EC is very important for effluent reuse considerations, since it is strongly related with salinity. Increased salinity can have a significant impact in terms of biokinetic as well as fouling behaviour in the MBR (Di Bella *et al.*, 2013). In this study, EC complied with the standards recommended for reuse (maximum 3 mS/cm) according to COEMA Resolution N<sup>o</sup> 2/2017 (Ceará, 2017).

# MBR performance

attributed to denitrification process.

Figure 5 (A) shows COD in the monitoring points 1, 2 and 3, where mean values were 6,837, 6,019 e 196 mgO<sub>2</sub>.L<sup>-1</sup>, respectively. Average overall COD removal efficiency (from MP1 to MP3) was about 97.1%. Moore (2015) also reported similar results when studying the performance of an MBR (bench scale) on the treatment of fruit (and other vegetables) industries: 97.0% COD removal. Fraga *et al.* (2017) found COD removal efficiency of 94.1% when studying an MBR treating dairy industry wastewater. Belli (2015), when studying an MBR treating sanitary wastewater, also reported COD removal efficiency of 97.0%. Therefore, the removal efficiency herein found is in accordance with literature results.

Figure 6 (A) shows  $BOD_5$  in the three monitoring points (MP1, MP2 and MP3), where mean values were 3,730, 3,238 and 42 mgO<sub>2</sub>.L<sup>-1</sup>, respectively. Average overall  $BOD_5$  removal efficiency (from MP1 to MP3) was 98.7%, higher than the requested value of up to 60% as recommended by CONAMA Resolution 430 (Brasil, 2011). Thus, the removal efficiency for  $BOD_5$  herein found is in



accordance with literature results, where Moore (2015) reached 99.9% BOD<sub>5</sub> removal in an MBR treating a fruit processing industry wastewater, and Fraga *et al.* (2017) found BOD<sub>5</sub> removal efficiency of 98.1% when studying an MBR treating dairy industry effluent.

High efficiency for both COD and BOD<sub>5</sub> were kept even for high organic loads, showing good capacity of the MBR to resist to such picks.



Figure 5. COD concentration in the three monitoring points (A) and removal efficiencies (B).



Figure 6. BOD<sub>5</sub> concentration in the three monitoring points (A) and removal efficiencies (B).



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Figure 7 (A) shows total nitrogen (TN) concentration in the three monitoring points, where mean values were 39.9 and 4.4 mg.L<sup>-1</sup> for MP1 and MP3, respectively. Figure 7 (B) shows removal efficiency for TN in the MBR system. Average overall TN removal efficiency (from MP1 to MP3) was 95.7%. Fraga et al. (2017) also found TN removal efficiency (93.1%) similar to the present study.

Figure 8 (A) shows total phosphorus (TP) concentration in the three monitoring points, where mean values were 13.5 and 8.5 mg.L<sup>-1</sup> for MPs 1 and 3, respectively. Figure 7 (B) shows removal efficiency for TP in the MBR system. The mean global removal efficiency for TP was 53.5%. It must be stated that the removal efficiency for TN and TP is even higher than 95.7% and 53.5%, respectively, since nitrogen (as urea) and phosphorus (as phosphoric acid) were added in the MLSS as nutrient source for bacterial growth.

Moore (2015) reported TP removal efficiency of 60% when studying a MBR applied to the treatment of fruit (and other vegetables) industries, which is higher than the result herein found.

With regard to microbiological content, both total coliform and *E.coli* were absent in both monitoring points (MP1 and MP3). This confirms that sanitary wastewater is not connected to the industrial wastewater stream. Subtil *et al.* (2013), when studding an MBR treating sanitary wastewater found that microbiological content, in terms of total coliform and *E.coli* was compatible with unrestricted urban reuse of the treated wastewater. Therefore, whether these bacteria were present in the industrial wastewater, they are expected to be efficiently removed by the ultrafiltration membranes.



Figure 7. TN concentration in the three monitoring points (A) and removal efficiencies (B).



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Figure 8. TP concentration in the three monitored points (A) and removal efficiencies (B).

### Effluent reuse according to Brazilian standards

Permeate quality attended the recommendation of NBR 13.969 (ABNT, 1997) for reuse in class I (car washing), class II (floor washing, garden watering and ornamental purposes), class III (toilet flushing) and class IV (irrigation of fruit tree, cereals and forage crops) and COEMA Resolution 2/2017 (Ceará, 2017) for all reuse categories (urban reuse, agriculture and forest reuse, environment reuse, industry reuse, aquaculture reuse). Because permeate was absent from both total coliform and *E.coli*, it can be reuse for unrestricted irrigation according to World Health Organization (WHO, 2006). Therefore, permeate produced in the MBR herein reported, can be reuse in a variety of usages, including some in the industry where it was located.

#### Conclusions

MBR showed to be very efficient on the removal of COD, BOD<sub>5</sub>, total nitrogen and total phosphorus from a fruit processing industry wastewater. Removal efficiencies for BOD<sub>5</sub> attended Brazilian legislation for effluent discharge. MBR also showed good resilience, since high efficiencies were maintained regardless the high organic loads.

Permeate quality was found to be in accordance with Brazilian reuse standards recommended in NBR 13.969 (ABNT, 1997) and COEMA Resolution 2 (Ceará, 2017) for a variety of uses, such as: car washing, floor washing, garden watering, ornamental purposes, environmental restoration, toilet flushing, irrigation of fruit tree, cereals and forage crops, aquaculture and industrial uses.

Application of MBR technology can therefore contribute to water saving in the industry herein reported, since the final effluent is suitable for reuse in several common activities in the industrial sector.



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